



Siena Hurwitz¹, Matt Landreman¹, Thomas M. Antonsen¹
¹University of Maryland, College Park

Introduction

- Lorentz forces are a key coil engineering design parameter for magnetic confinement fusion reactors
- Lorentz forces are generally evaluated slowly with finite element analysis codes
- It is desirable to evaluate the forces rapidly to facilitate integration with physics design
- A simple filamentary approximation for $d\mathbf{F}/d\ell$ with the Biot-Savart law fails as the result diverges logarithmically

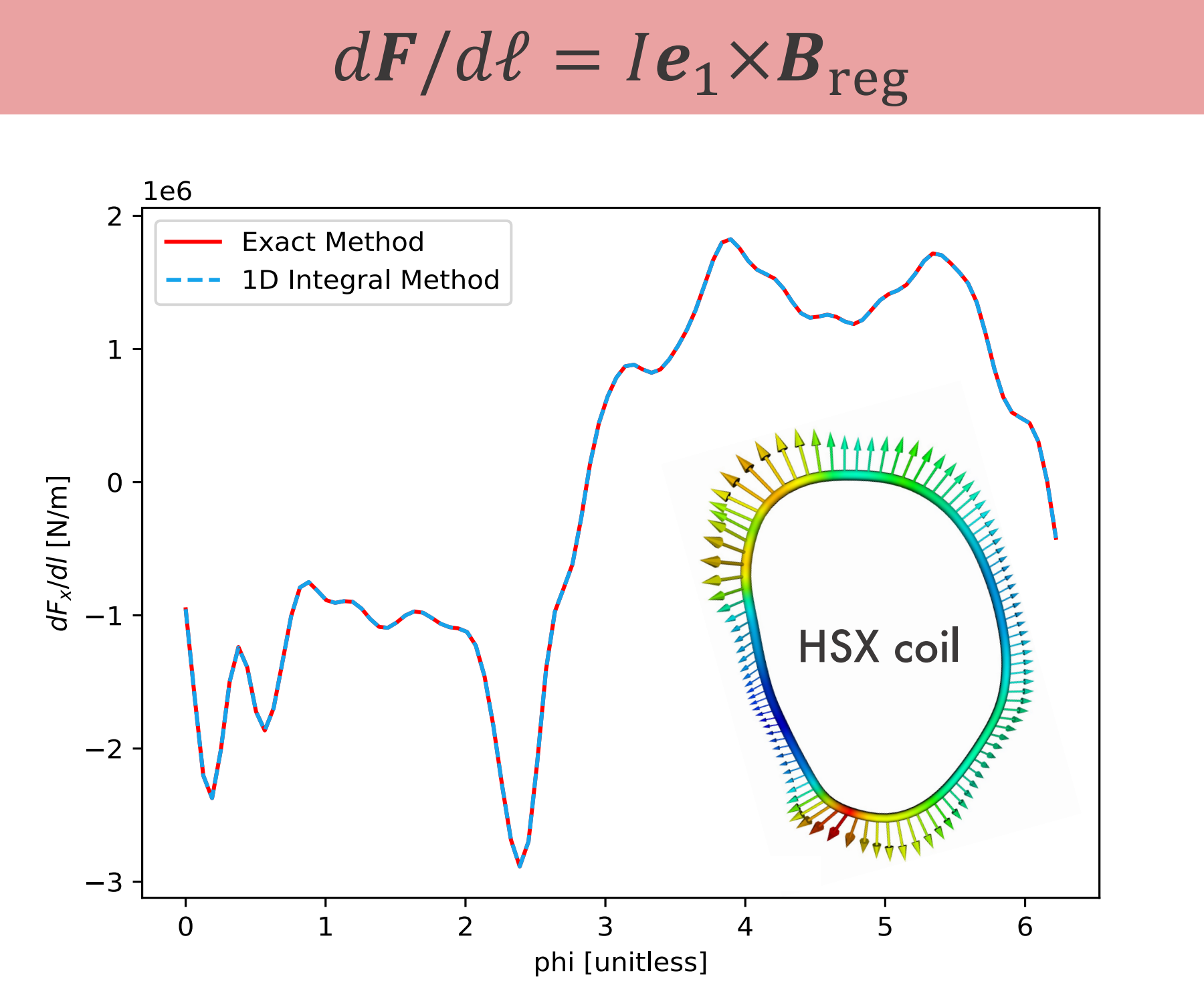
Reduced Model Derivation

- Construct a quasi-cylindrical coordinate system from the coil center-line, \mathbf{r}_c , and the Frenet-Serret unit vectors, $\{\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3\}$,
 $\mathbf{r}(s, \theta, \phi) = \mathbf{r}_c + s \cos \theta \mathbf{e}_2 + s \sin \theta \mathbf{e}_3$
 $(\mathbf{e}_1 = \mathbf{r}'_c/|\mathbf{r}'_c|, \mathbf{e}_2 = \mathbf{e}'_1/|\mathbf{e}'_1|, \mathbf{e}_3 = \mathbf{e}_1 \times \mathbf{e}_2)$
- Assume uniform current density and a circular cross-section
- Express the magnetic vector potential and Lorentz force in the system,

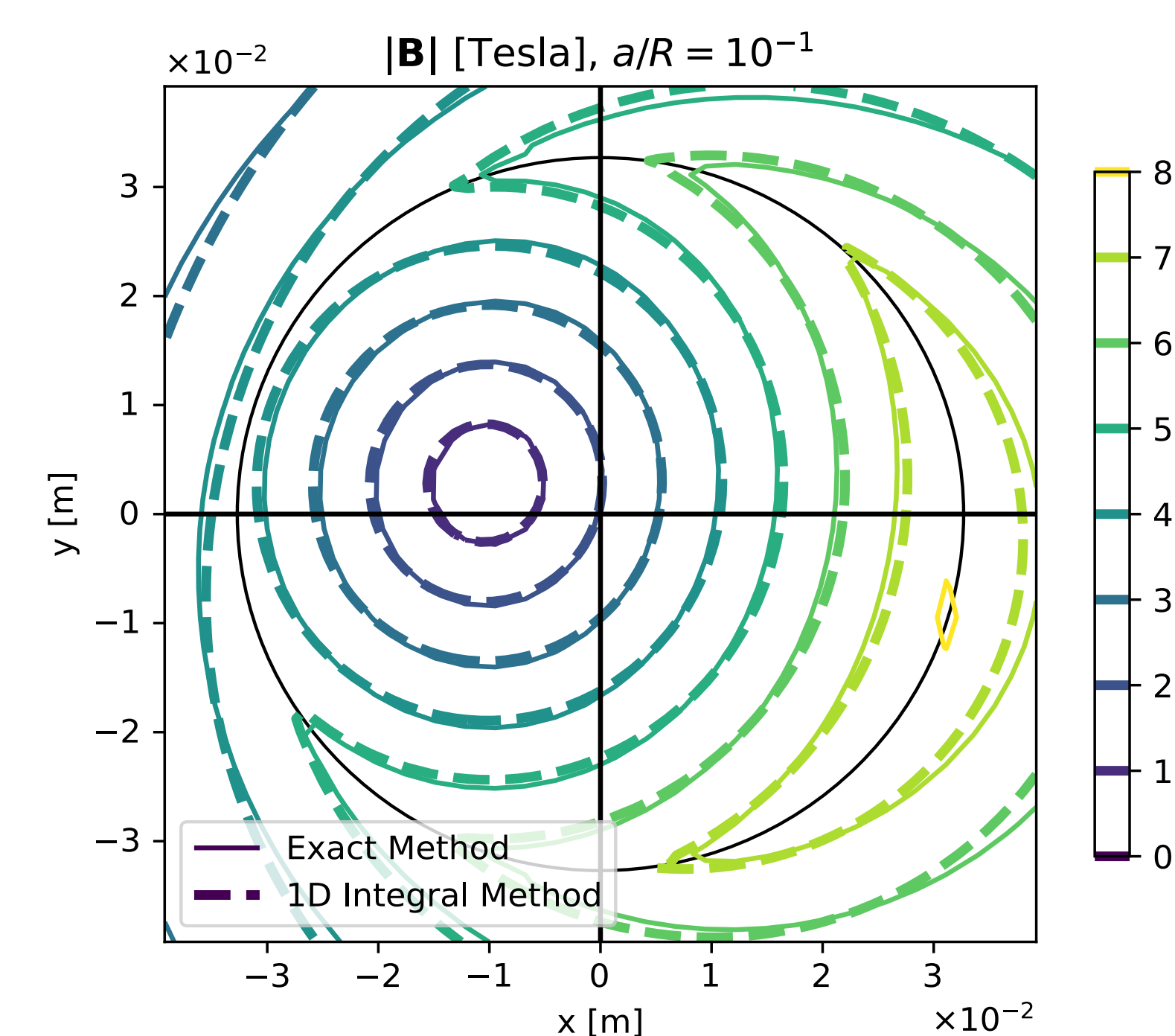
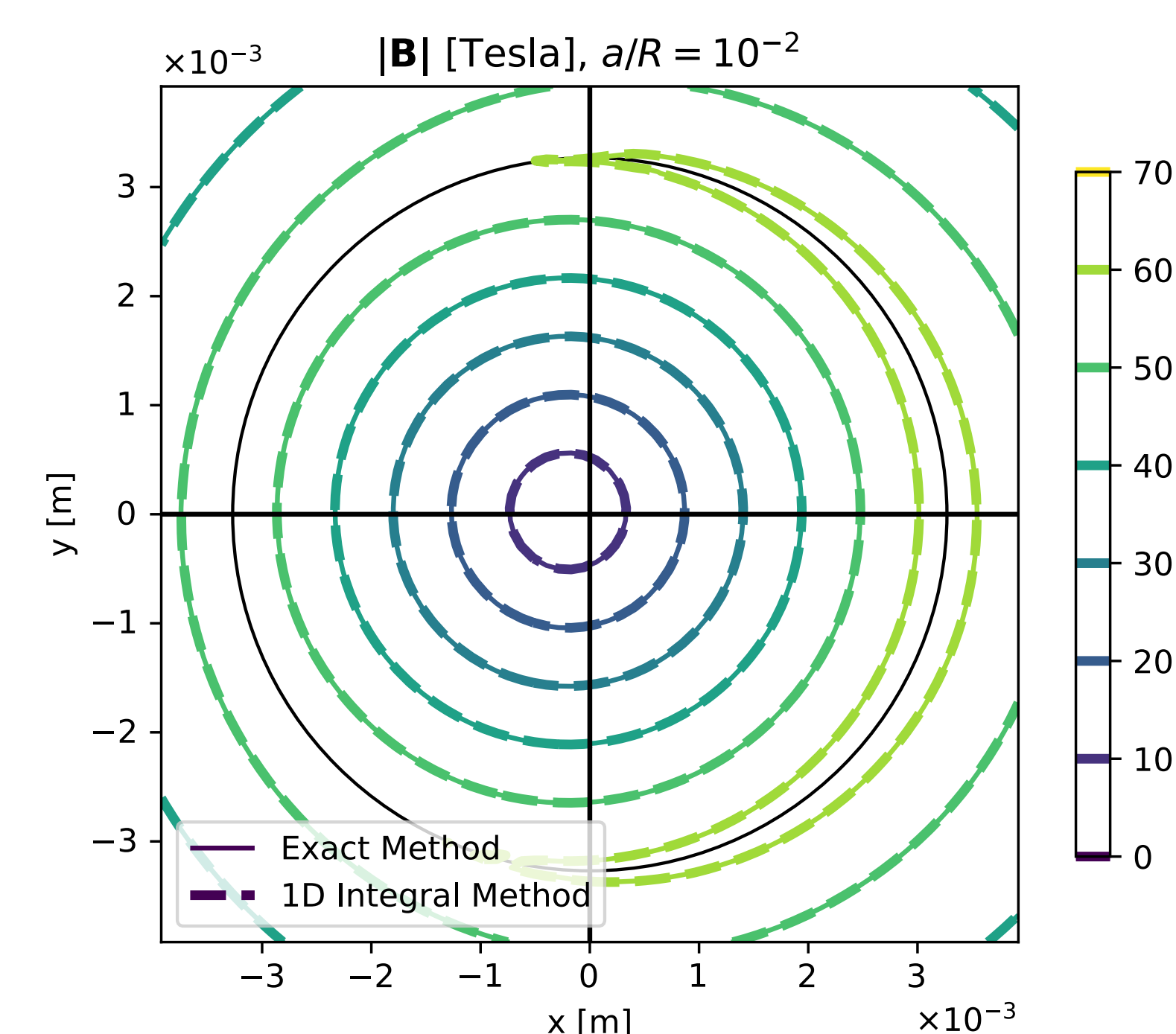
$$A(\mathbf{r}) = \frac{\mu_0 I}{4\pi a^2} \int_0^{2\pi} d\tilde{\phi} \int_0^{2\pi} d\tilde{\theta} \int_0^a d\tilde{s} \tilde{s} (1 - \tilde{\kappa}\tilde{s}) \frac{\tilde{\mathbf{r}}'_c}{|\Delta\mathbf{r}|}$$

$$\frac{d\mathbf{F}}{d\ell} = \frac{I}{\pi a^2} \int_0^{2\pi} d\theta \int_0^a ds s (1 - \kappa s) (\mathbf{e}_1 \times \mathbf{B})$$
- Assume $a/\mathcal{L} \ll 1$, where \mathcal{L} is a length scale of \mathbf{r}_c (e.g., $|\mathbf{r}'_c|, \kappa^{-1}$)
- Partition the integral over $\tilde{\phi}$ in $A(\mathbf{r})$ into two sections about ϕ_0 , where $a/\mathcal{L} \ll \phi_0 \ll 1$
 - The near region ($|\phi - \tilde{\phi}| < \phi_0$) satisfies $|\Delta\phi| \ll 1$
 - The far region ($|\phi - \tilde{\phi}| > \phi_0$) satisfies $a/|\Delta\mathbf{r}| \ll 1$
- Solve for $A(\mathbf{r})$ and simplify under these assumptions
- Posit a regularized form of the magnetic field, \mathbf{B}_{reg} , then calculate $\mathbf{B} = \nabla \times \mathbf{A}$ and $d\mathbf{F}/d\ell$ explicitly and compare to \mathbf{B}_{reg}

Reduced Model Results



$$\mathbf{B}(\mathbf{r}) = \mathbf{B}_{\text{reg}} + \mathbf{B}_{\text{cylinder}} + \mathcal{O}(\kappa s)$$



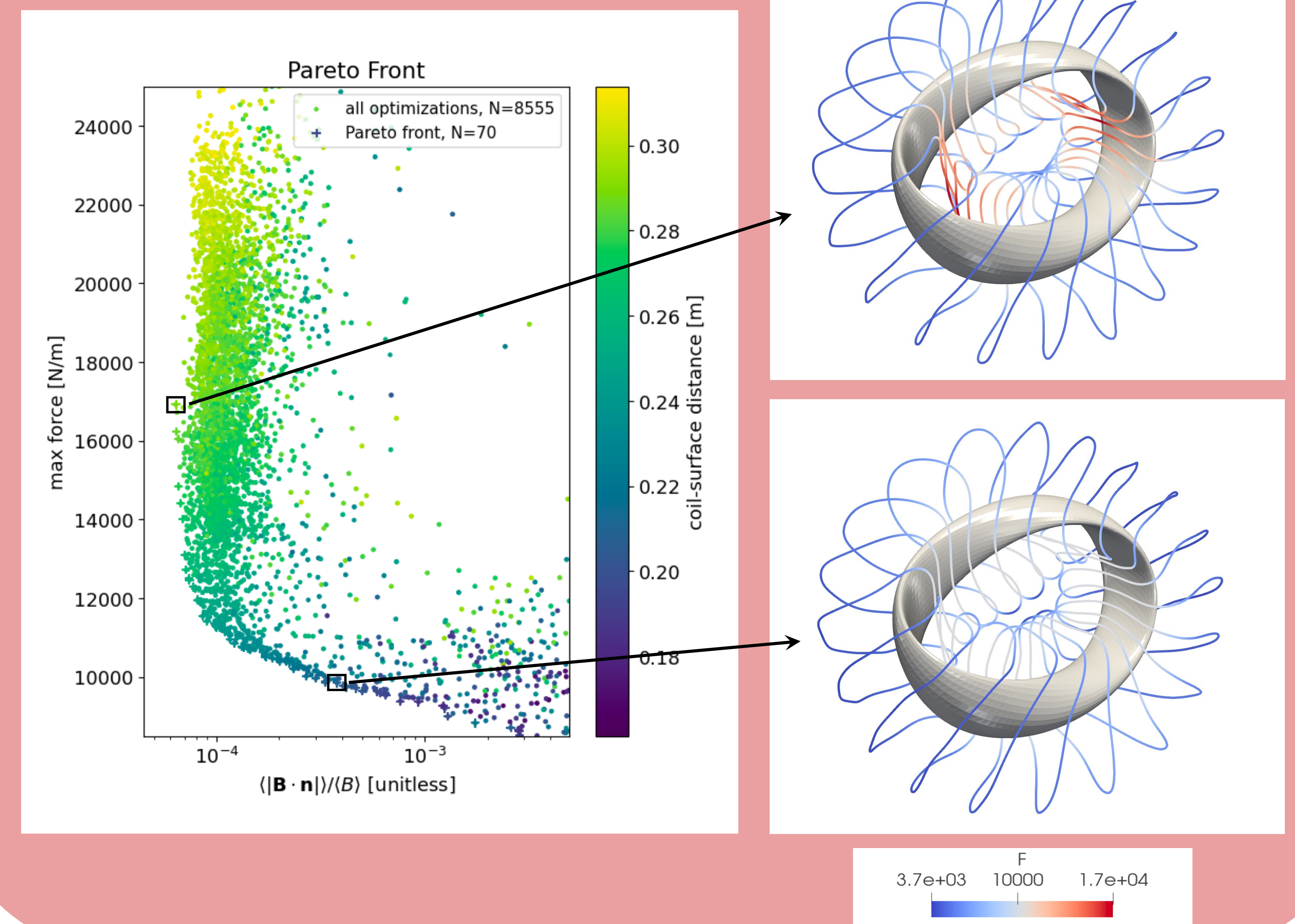
~10,000x faster than exact computations!

$$\mathbf{B}_{\text{reg}} = \frac{\mu_0 I}{4\pi} \int_0^{2\pi} d\tilde{\phi} \frac{\tilde{\mathbf{r}}'_c \times \Delta\mathbf{r}_c}{(|\Delta\mathbf{r}_c|^2 + a^2/\sqrt{e})^{3/2}}$$

Force Optimization Objective

- Optimized coils for the Landreman-Paul quasi-axisymmetric configuration, $N_{fp} = 2$
- Objective function penalizes
 - quadratic flux
 - arc length variance
 - coil-coil distance
 - Lorentz force
 - curvature
 - coil-surface distance
 - coil lengths
 - mean-squared curvature

Force Optimization Results



References

- Hurwitz, S., Landreman, M., & Antonsen Jr, T. M. (2023). Efficient calculation of self magnetic field, self-force, and self-inductance for electromagnetic coils. *arXiv:2310.12087*.
- Landreman, M., Hurwitz, S., & Antonsen Jr, T. M. (2023). Efficient calculation of self magnetic field, self-force, and self-inductance for electromagnetic coils. II. Rectangular cross-section. *arXiv:2310.12087*.